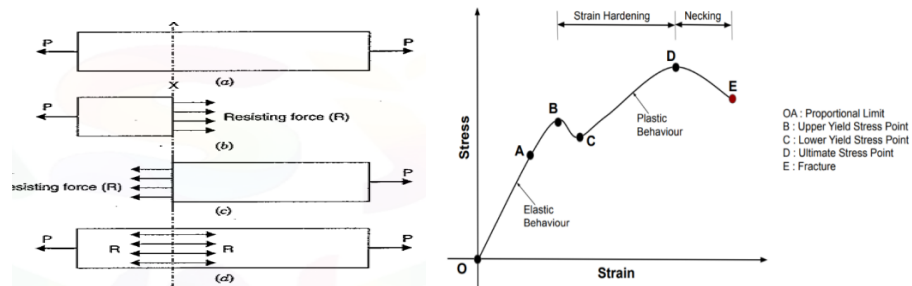


Unit-I.

Theories of failures

Theories of failures:

According to theory of failure a member is said to be fail if the member will not regain its original dimensions soon after removed applied load. (tensile/ compressive)



Principal stress:(σ)

The planes in the xyz system which have no shear stress and only subjected to normal stresses are known as Principal stresses.

Factor of Safety:

$$\frac{\text{Stress at elastic}}{\text{Principal Shear (or) Max Principal shear}}$$

Types of theories of failures:

- a) The Maximum Principal stress (or) Rankine's Theory
- b) The Maximum Principal Strain (or) St. Venant's theory
- c) The Maximum shear stress theory (or) Guest's theory
- d) The Maximum strain energy theory (or) Haigh's theory
- e) The maximum shear strain energy theory (or) Mises and von Mises theory

a. maximum principal stress theory (or) ranking's theory

According to this theory the failure will take place if $\sigma_1 \geq \sigma_t^*$ in Tension

$$\sigma_t = \sigma_1 : |\sigma_3| \geq \sigma_c \text{ in Compression} : \text{factor of safety} = \frac{\sigma_t}{\sigma_t^*} (\Rightarrow \sigma_1 = \sigma_t)$$

σ_1 = Principle Tensile Stress

σ_2 = Principle Tensile Stress

σ_3 = Principle compressive Stress

σ_t^* = shear at elastic limit

b. The Maximum Principal Strain (or) St. Venant's theory

According to this theory failure will take place if $e_1 \geq \frac{\sigma_t^*}{E}$; $|e_3| \geq \frac{\sigma_c}{E} \Rightarrow E = \frac{\sigma}{e}$
 young's modulus = $\frac{\text{stress}}{\text{strain}}$; Poisson ratio (μ) = $\frac{\text{lateral strain}}{\text{longitudinal strain}}$

$$e_1 = \frac{1}{E} [\sigma_1 - \mu (\sigma_2 + \sigma_3)] ; e_3 = \frac{1}{E} [\sigma_3 - \mu (\sigma_1 + \sigma_2)]$$

$$\frac{1}{E} [\sigma_1 - \mu (\sigma_2 + \sigma_3)] \geq \frac{1}{E} \sigma_t^* ; \frac{1}{E} [\sigma_3 - \mu (\sigma_1 + \sigma_2)] \geq \frac{1}{E} \sigma_c$$

$$\sigma_t = \sigma_1 - \mu (\sigma_2 + \sigma_3) ; \sigma_c = |\sigma_3 - \mu (\sigma_1 + \sigma_2)|$$

σ_1 = Principle Tensile Stress

σ_2 = Principle Tensile Stress

σ_3 = Principle compressive Stress

σ_t^* = shear at elastic limit

c. The Maximum shear stress theory (or) Guest's theory

According to this theory failure will take Place if $(\sigma_1 - \sigma_3) \geq \sigma_t^*$

maximum Shear stress = $\frac{1}{2} (\sigma_1 - \sigma_3)$ in Simple Tension $\sigma_2, \sigma_3 = 0$

$$\text{so } (\tau) = \left(\frac{1}{2} \sigma_t^* - 0\right) = \frac{1}{2} \sigma_t^* \quad \sigma_t = (\sigma_1 - \sigma_3)$$

σ_1 = Principle Tensile Stress

σ_2 = Principle Tensile Stress

σ_3 = Principle compressive Stress

σ_t^* = shear at elastic limit

d. The Maximum strain energy theory (or) Haigh's theory

According to this failure will take place if $\sigma_1^2 + \sigma_2^2 - 2\mu (\sigma_1 * \sigma_2) \geq \sigma_t^2$

Modules of elasticity (E) = $\frac{\sigma}{e} = \frac{\text{stress}}{\text{strain}}$

Strain (e) = $\frac{\delta L}{L} = \frac{\text{change in length}}{\text{original length}}$; Volume = Area * Length

Stress (σ) = $\frac{P}{A} = \frac{\text{Load}}{\text{Area}}$; Strain energy in a body (u) = Work done by load (p)

$$= \frac{1}{2} * p * \delta L ; = \frac{1}{2} * (\sigma * a) * (l * e) ; = \frac{1}{2} * \sigma * e * Al$$

$$= \frac{1}{2} * \sigma * e * \text{volume}$$

So, Strain energy Per unit Volume

$$= \frac{1}{2} * \sigma * e = \frac{1}{2} * \text{stress} * \text{strain}$$

So total strain energy per unit volume $U = \frac{1}{2}\sigma_1 * e_1 + \frac{1}{2}\sigma_2 * e_2 + \frac{1}{2}\sigma_3 * e_3$

$$e_1 = \frac{1}{E}[\sigma_1 - \mu(\sigma_2 + \sigma_3)]; \quad e_2 = \frac{1}{E}[\sigma_2 - \mu(\sigma_1 + \sigma_3)]; \quad e_3 = \frac{1}{E}[\sigma_3 - \mu(\sigma_1 + \sigma_2)];$$

submitted in above equation

strain energy at elastic limit

$$= \frac{1}{2} * (\sigma_t^*) * (e_t^*)$$

$$= \frac{1}{2E} (\sigma_t^*)^2 * [E = \frac{\sigma}{e}]$$

$$\sigma_t^2 = \sigma_1^2 + \sigma_2^2 - 2\mu(\sigma_1 * \sigma_2)$$

$$U = \frac{1}{2E} [\sigma_1^2 + \sigma_2^2 + \sigma_3^2 - 2\mu(\sigma_1\sigma_2 + \sigma_2\sigma_3 + \sigma_3\sigma_1)]$$

e. maximum strain energy theory

According to this failure will take place if $(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \geq (2\sigma_t^*)^2$

$$\text{total shear strainenergy} = \frac{1}{2c} (\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2$$

In tension $\sigma_2, \sigma_3 = 0$

$$= \frac{1}{2c} [2\sigma_t^{*2}]$$

σ_1 = Principle Tensile Stress

σ_2 = Principle Tensile Stress

σ_3 = Principle compressive Stress

σ_t^* = shear at elastic limit

Problems on bolt design:

Given data:

Axial load (P) = 9 KN = 9000N

Shear force (f) = 4.5 KN = 4500N

Shear at elastic limit in tension

$$\sigma_t^* = 225 \text{ N/mm}^2$$

Factor of safety = 3

Poisson ratio = 0.3

Data: -

Diameter of bolts = (d) mm

- Factor of safety

$$\begin{aligned} &= \frac{\sigma_t^*}{\sigma_t} \\ \sigma_t &= \frac{\sigma_t^*}{F_s} \\ &= \frac{225}{3} \\ &= 75 \text{ N/mm}^2 \end{aligned}$$

- tensile stress (σ) = $\frac{P}{A}$
 $= \frac{9000}{\frac{\pi}{2}(d^2)} = \frac{9000}{(d^2)} \text{ N/mm}^2$
- shear stress (τ) = $\frac{f}{\frac{\pi}{2}(d^2)}$

$$\frac{4500}{\frac{\pi}{2}(d^2)} = \frac{4500}{(d^2)} \text{ N/mm}^2$$

- max/min principal stresses $= \frac{\sigma}{2} \pm \sqrt{\left(\left(\frac{\sigma}{2}\right)^2 + \tau^2\right)}$
 $= \frac{11459}{2(d^2)} \pm \sqrt{\left(\left(\frac{11459}{2d^2}\right)^2 + \left(\frac{5729.5}{d^2}\right)^2\right)}$

By solving

$$\sigma_1 (+) = \frac{1382.5}{d^2} \text{ N/mm}^2$$

$$\sigma_2 (-) = -\frac{2373.5}{d^2} \text{ N/mm}^2$$

(Principal stress $\sigma_3 = 0$)

A. By using principal stress theory:

$$\begin{aligned}\sigma_1 &= \sigma_t \\ &= \frac{1382.5}{d^2} = 7 \\ \mathbf{D} &= \mathbf{13.6}\end{aligned}$$

B. By using principal strain theory

$$e = \frac{1}{E} [\sigma_1 - \mu (\sigma_2 + \sigma_3)]$$

$$e = \frac{1}{E} \left[\frac{13832.51}{d^2} - 0.3 \left(-\frac{2378.5}{d^2} \right) + 0 \right]$$

$$\Rightarrow \frac{1}{E} \left(\frac{14554.65}{d^2} \right)$$

$$\Rightarrow e = \frac{\sigma_t}{E} \Rightarrow \frac{75}{E}$$

$$\Rightarrow \frac{14544.55}{d^2 E}$$

$$\Rightarrow \mathbf{d = 14mm}$$

c. By using maximum shear Theory

$$\tau = \frac{1}{2} (\sigma_1 - \sigma_2)$$

$$\tau = \frac{1}{2} \left[\frac{13832.5}{d^2} - \left(-\frac{2373.5}{d^2} \right) \right]$$

$$\Rightarrow \frac{8103}{d^2} \text{ N/mm}^2$$

$$\frac{1}{2} (\sigma_t - 0) = \frac{\sigma_t}{2} = \frac{75}{2} = 37.5$$

$$\text{Equating } 37.5 = \frac{8103}{d^2}$$

$$\mathbf{D = 15 mm}$$

d. By using shear strain energy theory

$$\sigma_1^2 + \sigma_2^2 - 2\mu (\sigma_1 * \sigma_2) = \sigma_t^2$$

$$\left[\frac{13832.5}{d^2} \right]^2 + \left[\frac{-2373.5}{d^2} \right]^2 - 2(0.3) (\sigma_1 * \sigma_2) = 75^2$$

$$\text{By solving } \mathbf{d = 14.01 mm}$$

e. By maximum shear strain energy theory

$$(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 = 2\sigma_t^2$$

$$\mathbf{D = 14.213 mm}$$